

(Submitted to PASJ)

# Comparing Explodability Predictions from a Parameter-Optimized Semi-Analytic Model with Structure-Based Progenitor Criteria

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# 1. INTRODUCTION

Motivation: 3D is more reliable, but 1D remains the “large-sample workhorse.”

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**3D** realistic, but are computationally expensive. Difficult to cover large progenitors samples.

Practical applications (e.g. yield grids, galactic chemical evolution, and light-curve/spectral inference) still rely on **1D**

**The key challenge:**

Do traditional structure-based criteria truly represent the underlying explosion physics?

How can we use a limited set of 3D models to constrain the parameters of a fast 1D model?

**Our strategy:**

Calibrate a semi-analytic 1D model (**Muller et al., 2016**) using 3D results (**Burrows et al. 2024**).

Use calibrated model to rigorously compare structure-based criteria.

# 2. METHOD: MÜLLER MODEL

Semi-analytic 1D model: approximating multi-D effects with interpretable parameters

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## TUNABLE PARAMETERS

### Framework:

Müller et al. (2016),  
revisions by Takahashi et al. (2023).

### Explosion criterion:

based on timescale ratio  $\tau_{\text{adv}}/\tau_{\text{heat}}$

### Outputs:

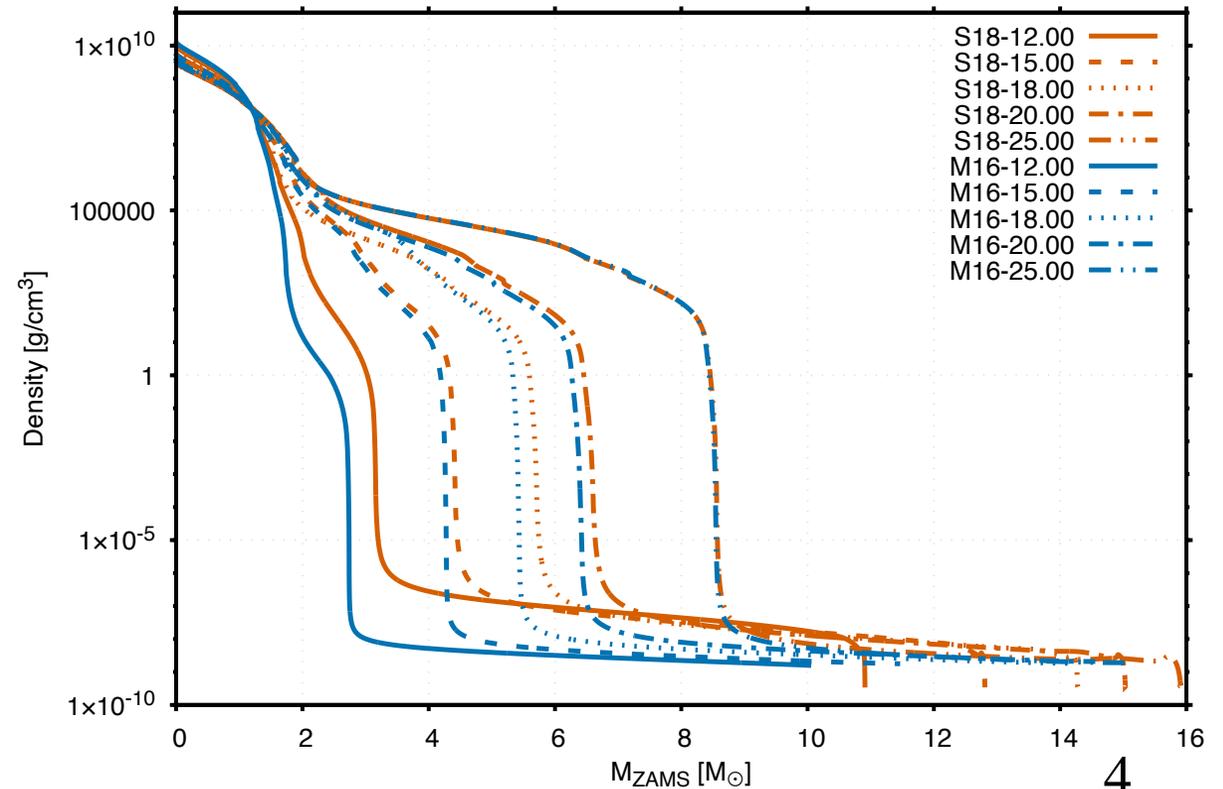
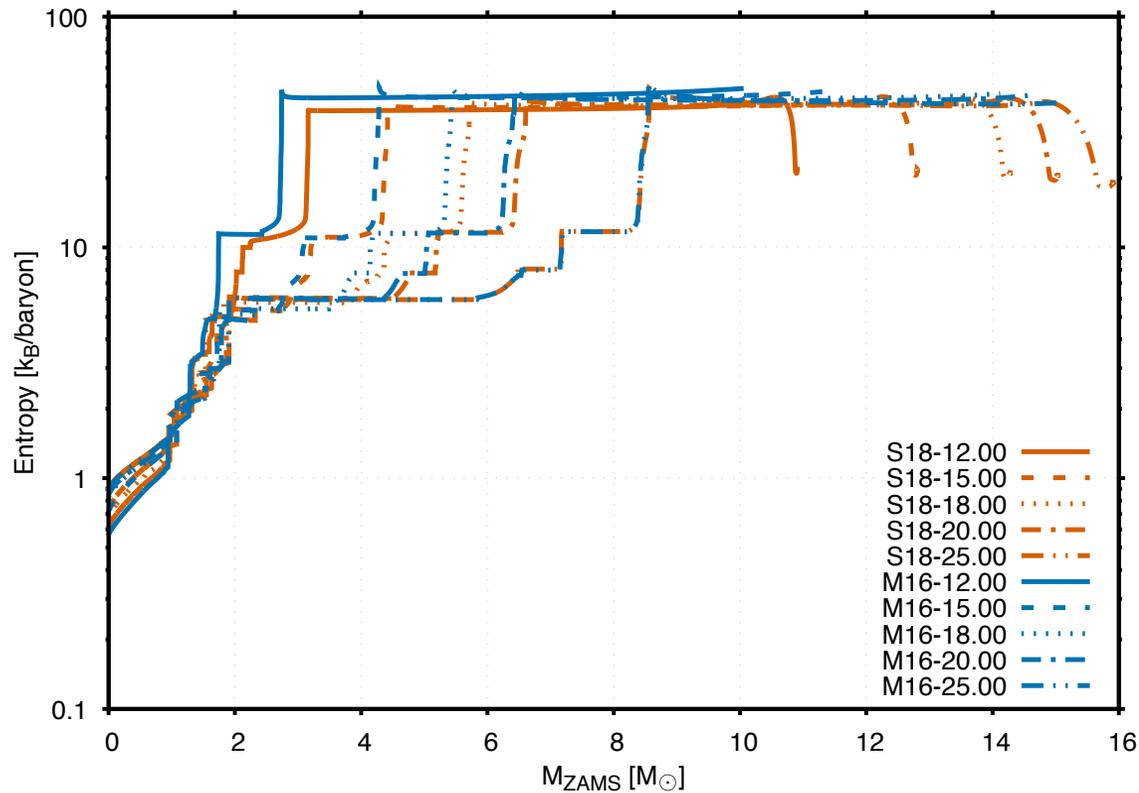
explodability, plus  $E_{\text{expl}}$ ,  $M_{\text{PNS}}$ , and  $M_{\text{Ni}}$ .

- $\alpha_{\text{turb}}$  Shock expansion factor due to turbulent stresses (Müller & Janka, 2015)
- $\zeta$  Efficiency factor for conversion of accretion energy into luminosity (Müller & Janka, 2014)
- $\tau_{1.5}$  Cooling time-scale for  $1.5 M_{\odot}$  neutron star (Hüdepohl, 2014)
- $\alpha_{\text{out}}$  Volume fraction of outflows
- $\beta_{\text{expl}}$  Shock compression ratio during explosion phase

# 2. METHOD: PROGENITOR SETS

Calibration data: FORNAX 3D sample and fitting targets

Progenitor set	Reference	Mass range [ $M_{\odot}$ ]	Minimum mass spacing [ $M_{\odot}$ ]
S16	Sukhbold et al. (2016)	9–120	0.1
S18	Sukhbold et al. (2018)	12–27	0.01
M16	Müller et al. (2016)	9.5–45	0.01



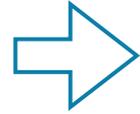
## 2. METHOD: OPTIMIZATION WORK

Calibration workflow: fit  $\alpha_{\text{turb}}(M_{\text{ff}})$  first, then jointly scan the remaining parameters

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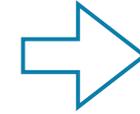
### STEP A

Scan  $\alpha_{\text{turb}}$  and minimize  
the single-model misfit  
 $\mathbf{x}_k^2$



### STEP B

Fit the best-fit  $\alpha_{\text{turb}}$   
values as a piecewise  
function of  $M_{\text{ff}}$  (free-fall  
mass coordinate)



### STEP C

Scan  $(\zeta, \tau_{1.5})$  within  
allowed ranges,  
then scan  $(\beta_{\text{expl}}, \alpha_{\text{out}})$ .

Misfit metric ( $\chi^2$ -like): simultaneously constrains three observables,

$$\begin{aligned} \chi_k^2 = & \left( \frac{E_{1\text{D},k} - E_{3\text{D},k}}{E_{3\text{D},k}} \right)^2 \\ & + \left( \frac{M_{\text{PNS},1\text{D},k} - M_{\text{PNS},3\text{D},k}}{M_{\text{PNS},3\text{D},k}} \right)^2 \\ & + \left( \frac{M_{\text{Ni},1\text{D},k} - M_{\text{Ni},3\text{D},k}}{M_{\text{Ni},3\text{D},k}} \right)^2, \end{aligned}$$

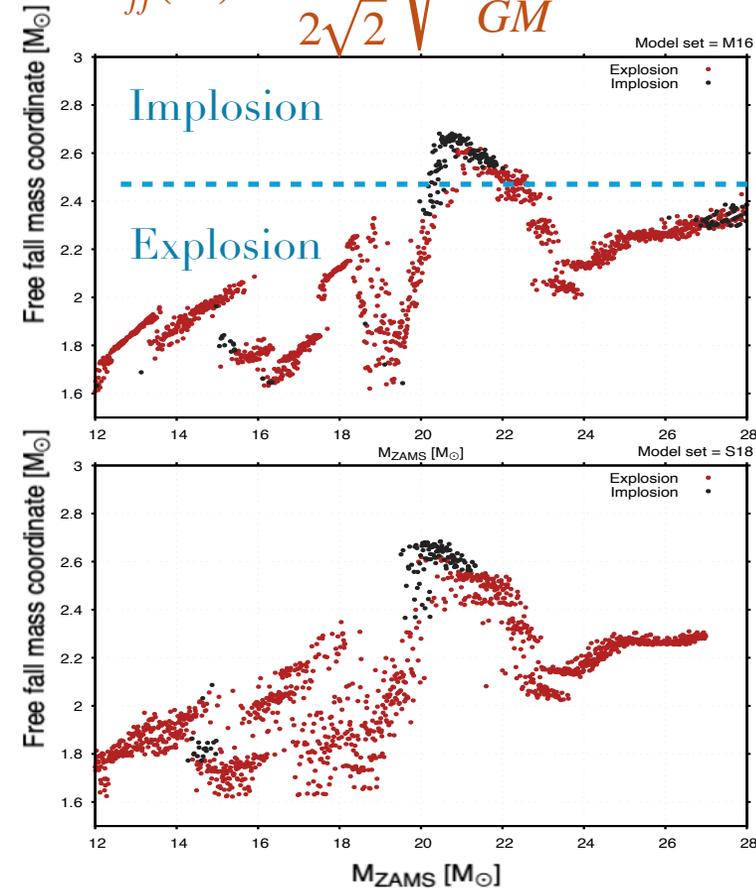
# 2. METHOD: STRUCTURE VARIABLES

Explodability: Structure-based progenitor criterion

## Free-fall Mass coordinate

K. Takahashi et al. (2023)

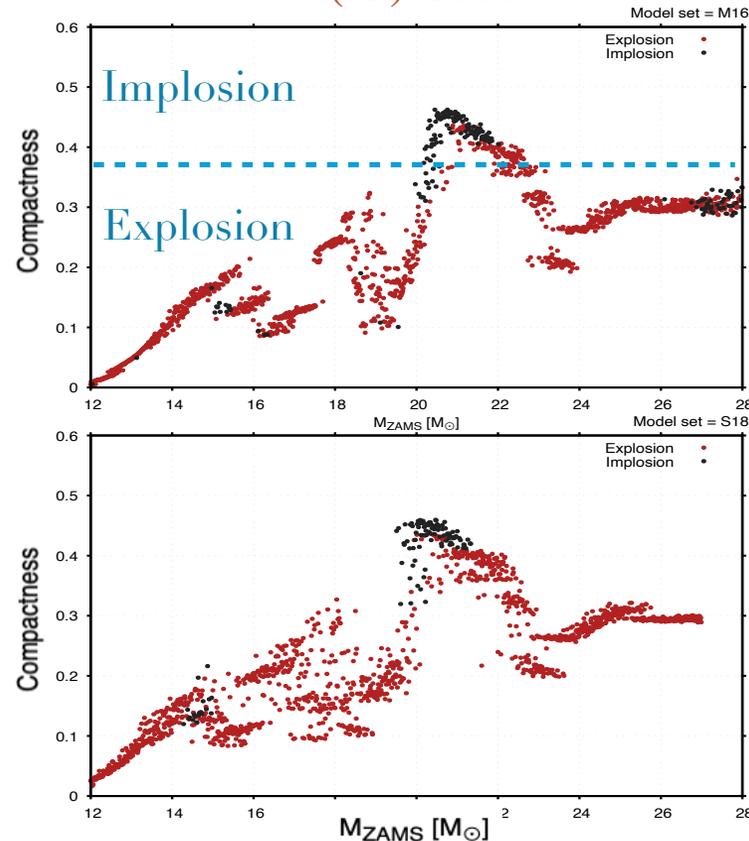
$$\tau_{ff}(M) = \frac{\pi}{2\sqrt{2}} \sqrt{\frac{R(M)^3}{GM}} = 1$$



## Compactness

E. O'Connor & C. D. Ott (2011)

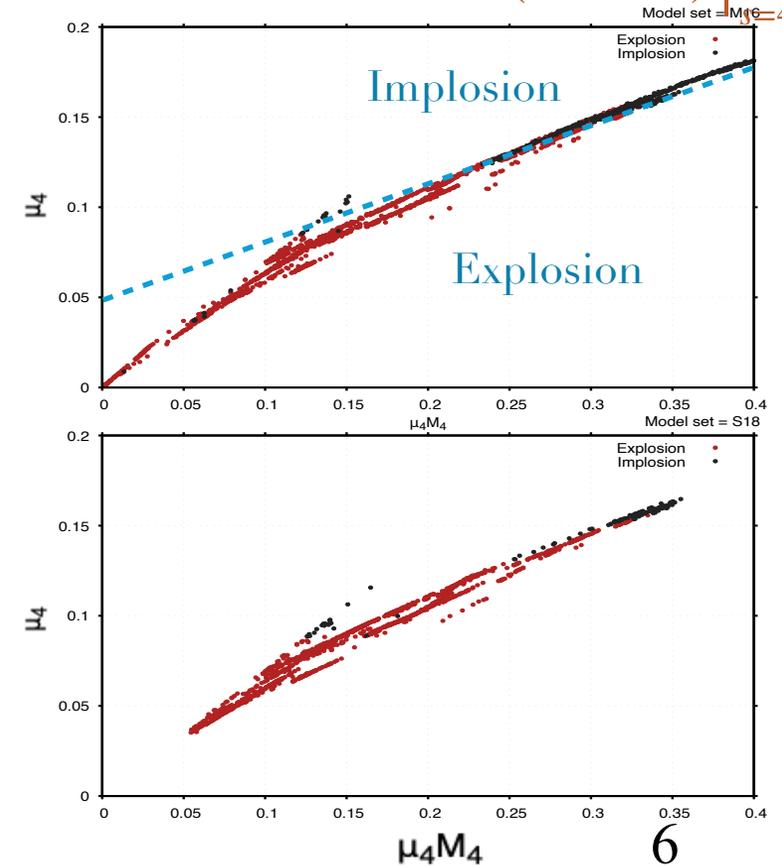
$$\zeta_M = \frac{M/M_{\odot}}{r(M)/1000\text{km}}$$



## Two-parameter criterion

T. Ertl et al. (2016)

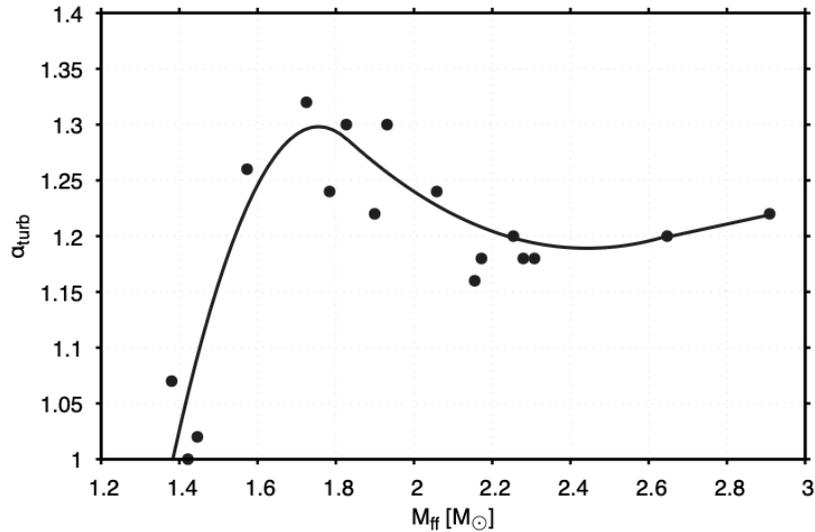
$$M_4 = m(s=4)/M_{\odot}, \mu_4 \equiv \frac{dm/M_{\odot}}{dr/(1000\text{km})}$$



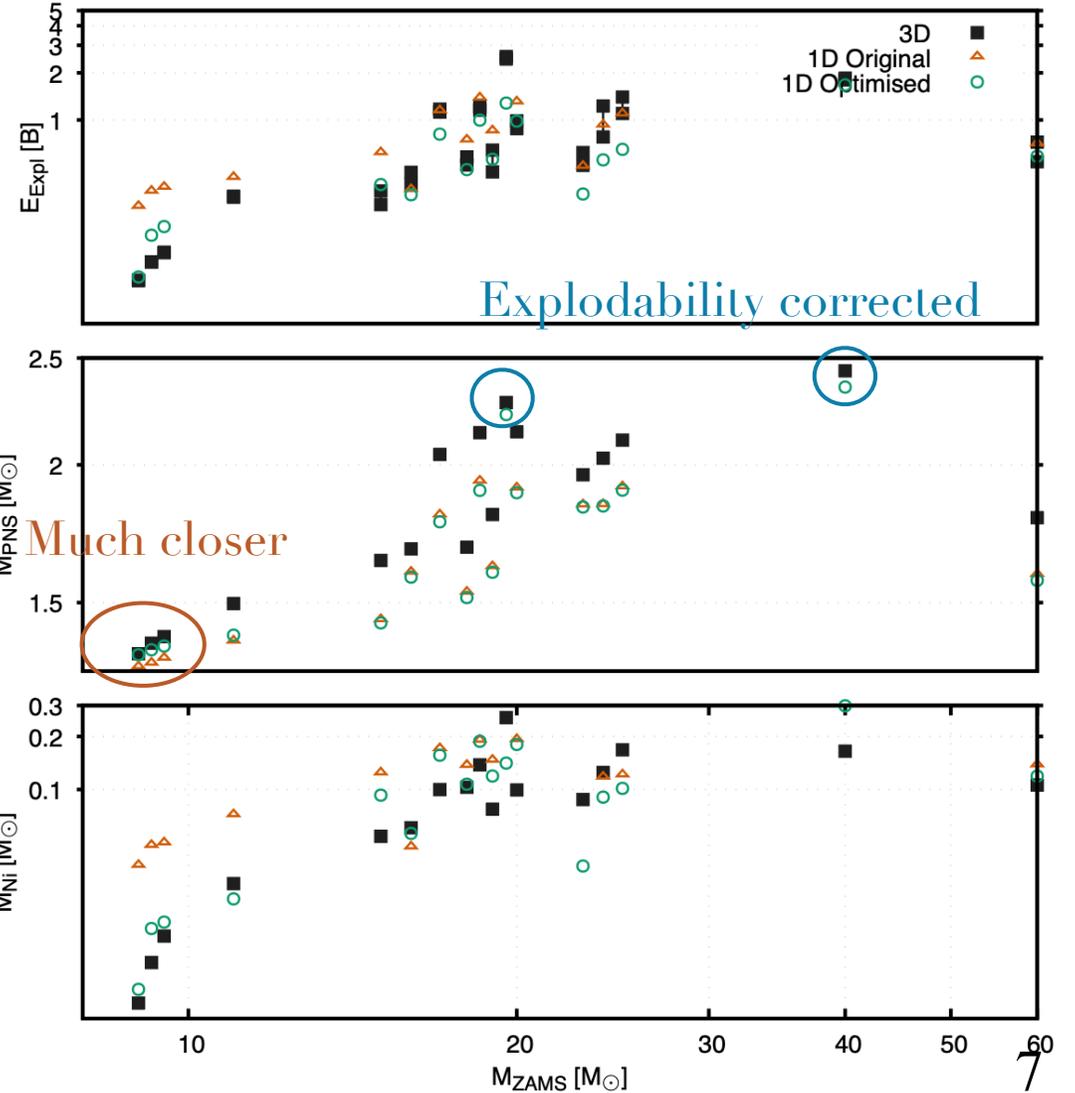
# 3. RESULTS & DISCUSSION

Result 4: Best-fit parameter set and improved overall agreement

Parameter	Original value	Optimized value
$\alpha_{\text{turb}}$	1.18	Piecewise functions related to $M_{\text{ff}}^{\dagger}$
$\zeta$	0.8	0.9
$\tau_{1.5}$	1.2	1.44
$\alpha_{\text{out}}$	0.5	0.32
$\beta_{\text{expl}}$	4	7



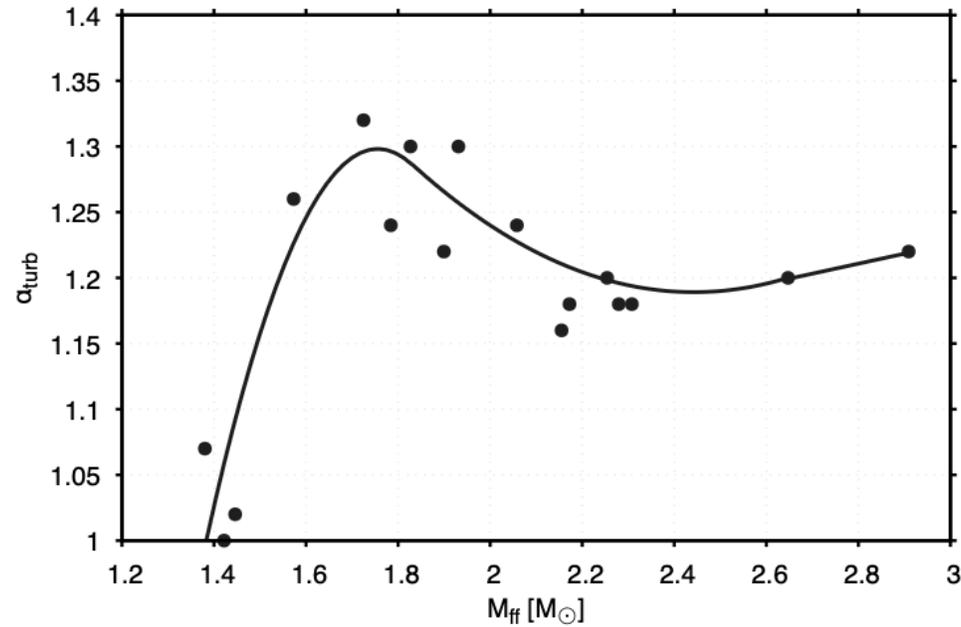
$\bar{\chi}^2_{\text{tot}}$  4.2  $\Rightarrow$  0.38



# 3.RESULTS & DISCUSSION

Result 3:  $\alpha_{\text{turb}}$  must vary systematically with progenitor structure

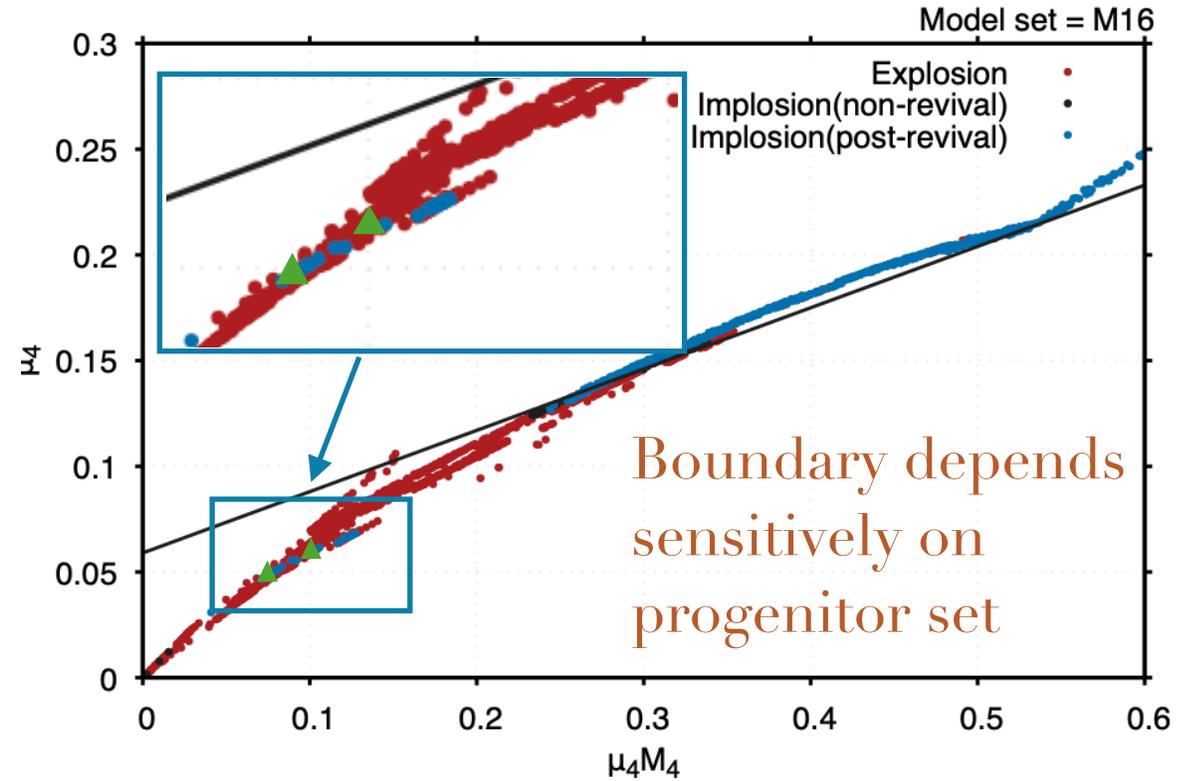
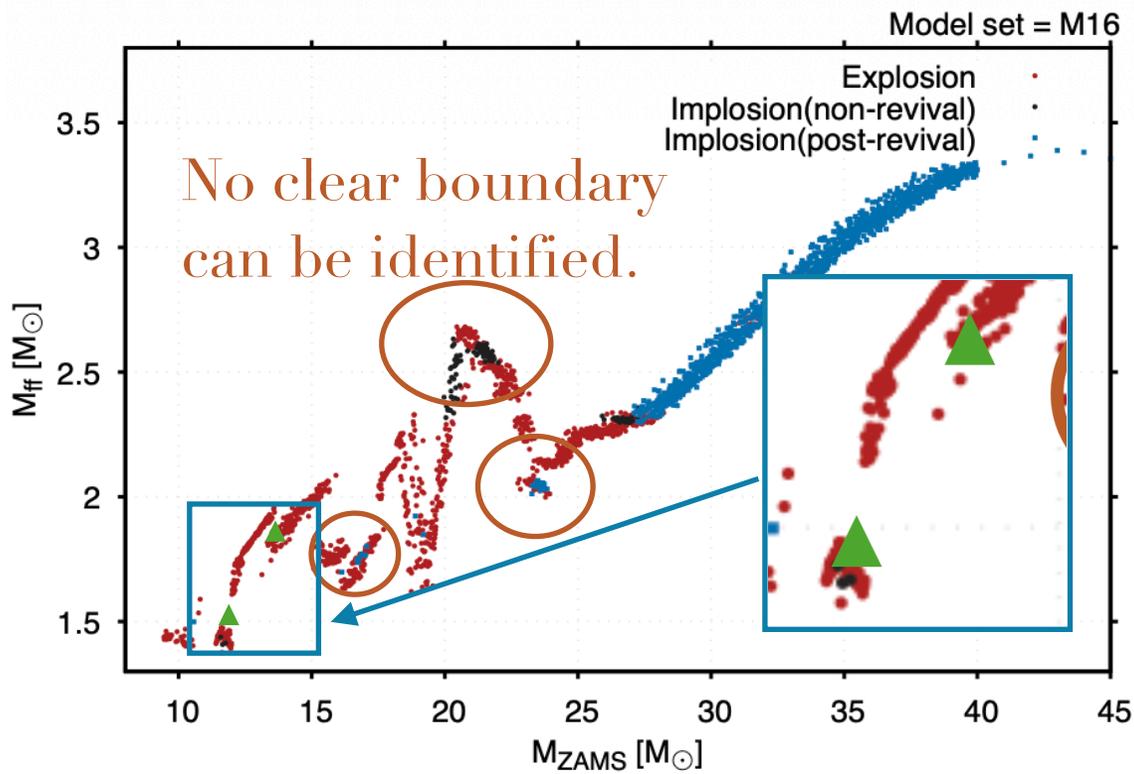
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Turbulence strength is governed by the balance between neutrino heating and accretion, varies systematically with progenitor structure.

# 3. RESULTS & DISCUSSION

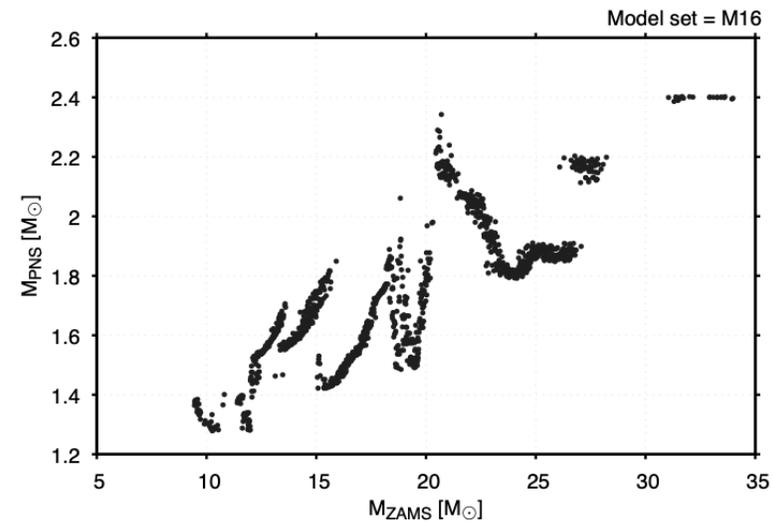
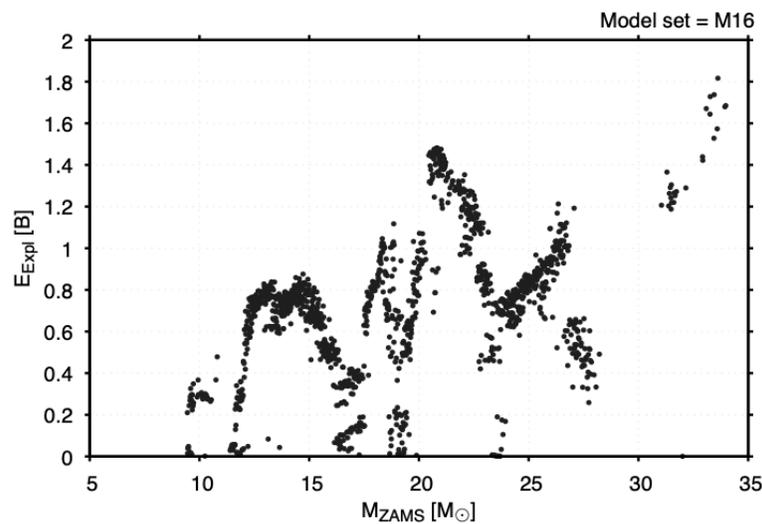
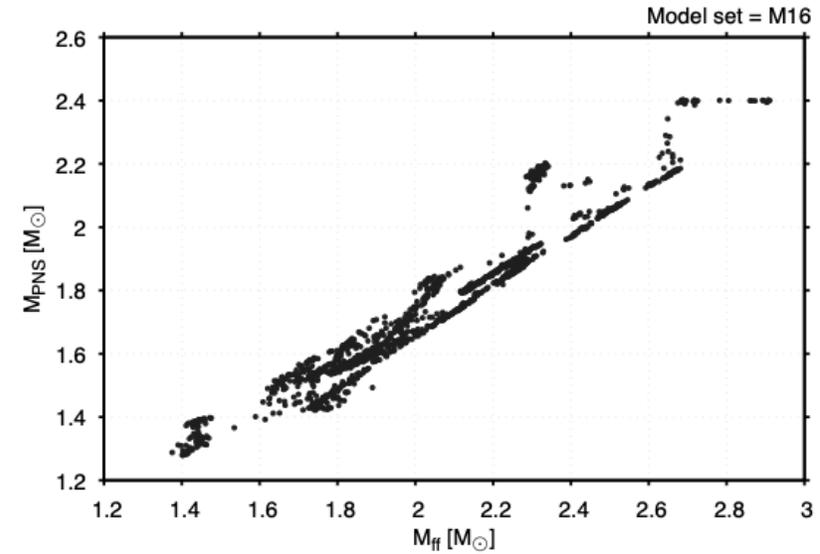
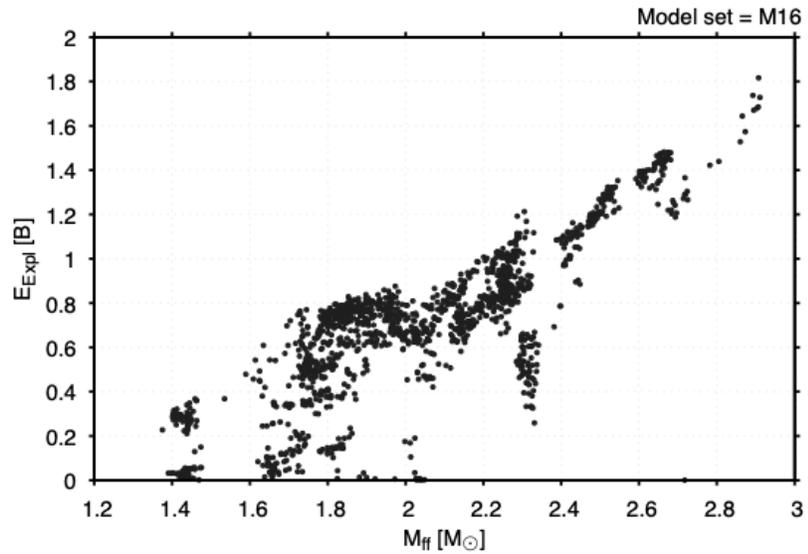
## Result 1: Reshaping of the explodability map



They may no longer be sufficient as a standalone predictor of explodability.

# 3.RESULTS & DISCUSSION

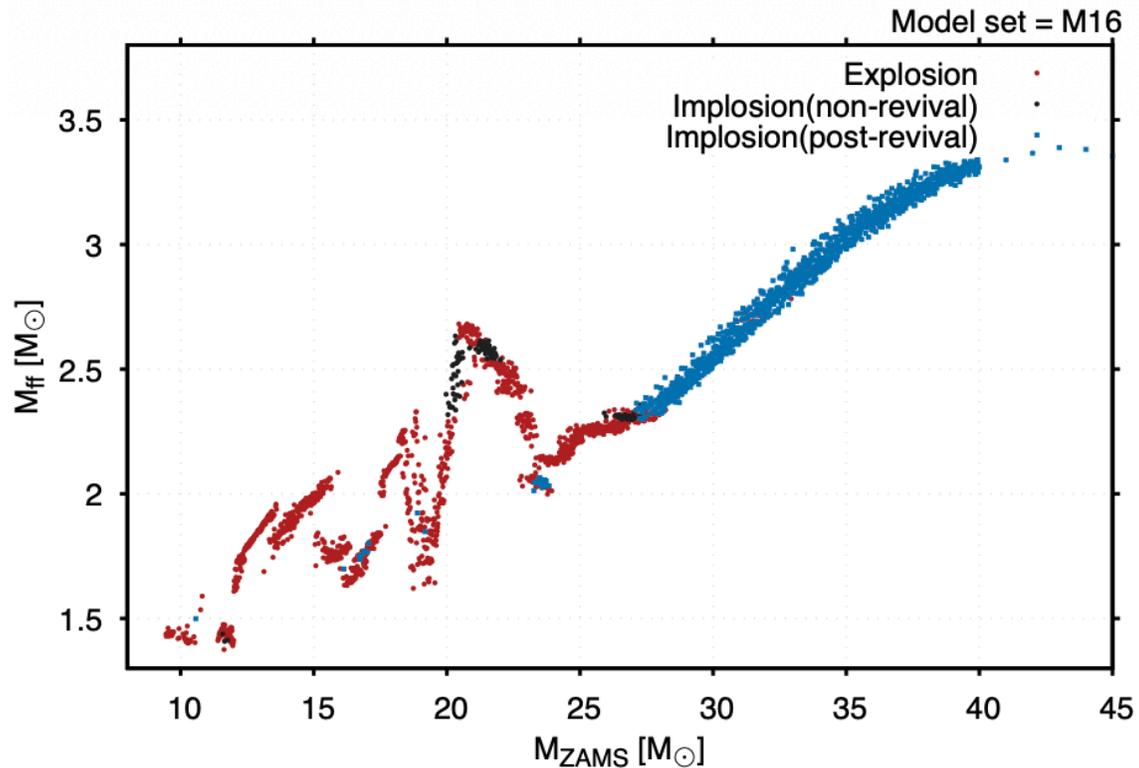
Result 2: monotonic correlation between explosion outcome and  $M_{\text{ff}}$



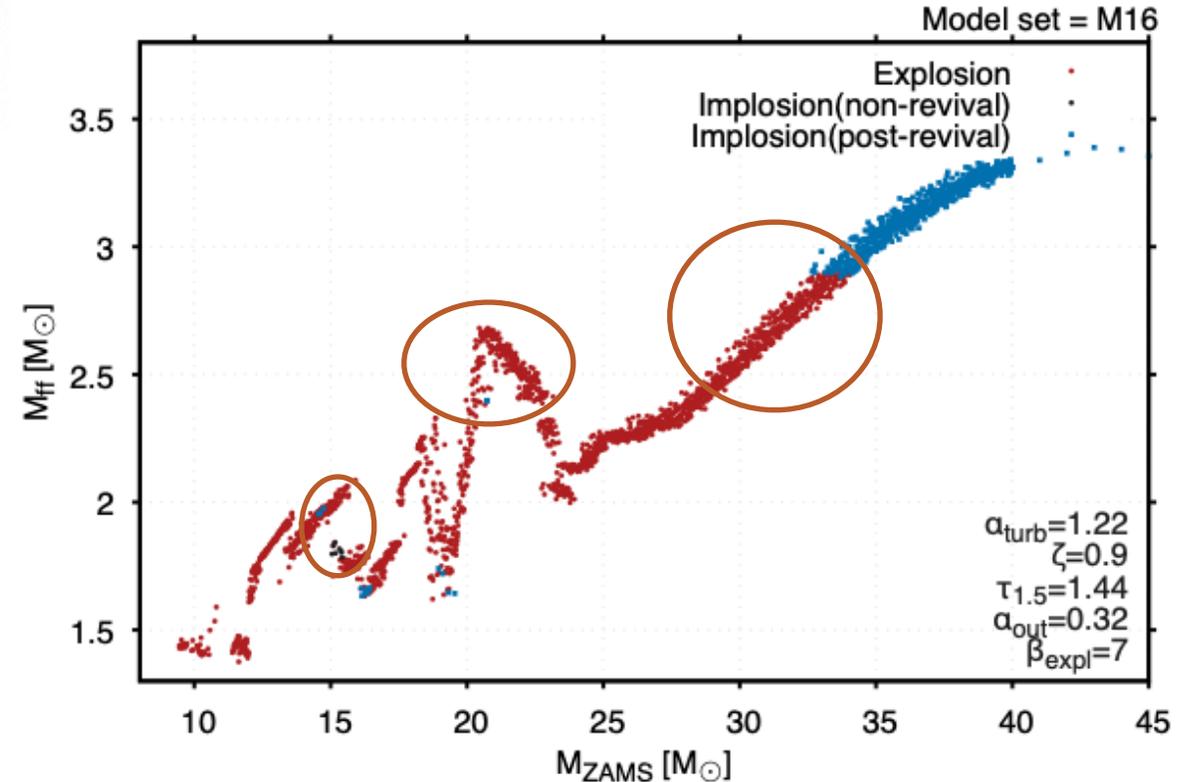
# 3.RESULTS & DISCUSSION

Result 3:  $\alpha_{\text{turb}}$  must vary systematically with progenitor structure

If  $\alpha_{\text{turb}}$  is fixed to a piecewise function



If  $\alpha_{\text{turb}}$  is fixed to a constant value



### 3. SUMMARY

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- A parameter-optimized semi-analytic 1D model can better reproduce 3D explosion trends than structure-based variables **while retaining computational speed.**
- Single-parameter structural diagnostics ( $M_{ff}$ ) are better suited as **trend indicators / ranking variables**, rather than universal explosion boundaries.
- Next steps: incorporate **more 3D calibration cases** and a **more physical treatment of late-time evolution**, to reduce parameter degeneracies and extrapolation uncertainties.